NADAR SARASWATHI COLLEGE OF ENGINEERING AND TECHNOLOGY, THENI.				
Course/Branch : B.E/ECE	Year / Semester : IV/ VII	Format No.	NAC/TLP-07a.13	
Subject Code : EC8701	Subject Name : Antennas and Microwave Engineering	Rev. No.	02	
Unit No : 5	Unit Name : Microwave Design Principle	Date	30.09.2020	
OBJECTIVE TYPE QUESTION BANK				

S. No.	Objective Questions (MCQ /True or False / Fill up with Choices)	BTL			
	The mask in a hybrid microwave circuit is made of:				
	a) rubylith				
1	b) silicon				
	c) quartz	112			
	d) arsenic				
	The metalized substrate is coaled with covered with the mast and exposed to				
	light source.				
2	a) photoresist				
	b) GaAs				
	c) germanium liquid				
	d) none of the mentioned				
	is a micromachining technique where suspended structures are formed on				
	silicon substrates.				
2	a) MMIC	T A			
5	b) HIC	L4			
	c) RF MEMS				
	d) none of the mentioned				
	In hybrid microwave integrated circuits, the various components of the circuit are etched in the				
4	substrate.	L5			
	a) true	13			
	b) false				
	Is defined as the ratio of power available from the two port network to the power available from the source				
	a) Transducer power gain				
5	b) Available power gain	L1			
	c) Power gain				
	d) None of the mentioned				
	Transducer power gain of a two port network is dependent on :				
	a) Z_S and Z_L				
6	b) Z _S	L1			
	c) Z_{L}				
	d) Independent of both the impedances				
	For a two port network the voltage reflection coefficient seen looking towards the load.				
	s is:				
	a) $(Z_{c} - Z_{a})/(Z_{c} - Z_{a})$				
7	h) $(Z_2 + Z_0)/(Z_2 - Z_0)$				
	$\begin{array}{c} 0 \\ c \\ c \\ \end{array} \begin{array}{c} 7 \\ c \\ \end{array} \begin{array}{c} 7 \\ c \\ c \\ \end{array} \begin{array}{c} 7 \\ c \\$				
	$\begin{array}{c} C \\ C $				
0	$\mathbf{u} \neq \mathbf{L} (\mathbf{v} \mid \mathbf{L} \mathbf{S} - \mathbf{L} (\mathbf{v}))$	T 1			
ð	In a two port network, the source impedance was measured to be 25 and the characteristic				
Prep	Prepared By: Mr.M.IDHAYACHANDRAN AP/ECEPage 1 of 5				

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	impedance of the transm at the source end is: a) -0.33333 b) -0.1111 c) 0.678 d) 0.2345	ission line was measured to be 50 . Then the second se	he reflection coef	ficient	
9	Gain of an amplifier is it a) True b) False Gain of a conjugate mate a) $R_{ds} (f_T)^2 / 4R_i (f)^2$ b) $4R_i (f)^2/R_{ds} (f_T)^2$	ndependent of the operating frequency.		L1 L3	
11	$\begin{array}{c} \text{c) } \text{R}_{\text{ds}}/\text{R}_{\text{i}} \\ \text{d) None of the mentioned} \\ \hline \\ \text{When both input and output of an amplifier are matched to zero reflection (in contrast to conjugate matching), the transducer power gain is: a) S21 \begin{array}{c} 2 \\ \text{b)} \\ \text{Sym} \end{array}$			to L2	
12	c) S_{12}^{2} d) $ S_{11}^{2}$ If the load impedance of then the reflection coeffi a) -0.111 b) -0.333 c) -0.987	T a two port network is 40 and the character cient of the two port network at the load end	eristic impedance	is 50 , L3	
13	 d) None of the mentioned High gain is not achieval a) device construction b) complex architecture c) ports are not matched d) none of the mentioned 	d ble at microwave frequencies using BJT amp d at high frequencies	olifiers because:	L1	
14	To flatten the gain response a) biasing current has to be b) input signal level has to c) increase the operational d) give negative feedback	e of a transistor: increased increased bandwidth to the amplifier	duced gain Dut thi	L1	
15	 a) balanced amplifiers b) distributed amplifiers c) differential amplifiers d) none of the mentioned 	a mat gain response is achieved at the cost of re- by using:	uuceu gain. But thi	L2	

a .		T 7 / O / T 7/TT77	Format	
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Co a) 16 b) c)	oupler that is mostly u branch line coupler wilkinson coupler lange coupler	sed in balanced amplifiers to achieve the requir	ed performant	ce is: L3
17 d) 17 d) 17 d) 10	waveguide coupler uses bala posite polarity at each differential amplifie distributed amplifier balanced amplifier none of the mentioned major advantage of d	nced input and output, meaning that there are 2 port. r	2 signal lines,	with L1
a) 18 b) c) d)	high gain low input impedance higher output voltag none of the mentioned	e swing		L5
19	are u diated power level. Power amplifiers Oscillators Transistors Attenuators	ised in the final stages of radar and radio transm	nitters to incre	L1
m a) 20 b) c) d)	Efficiency Gain Thermal effect All of the mentioned	onsidered for power amplifier design are:		LI
G a) 21 b) c) d)	ain of power amplifier Increases Decreases Increases exponential Decreases exponentia	s with increase in operating freque pering & Technology ly		L2
22	amplifiers ver the entire range of the class A amplifiers Class B amplifiers Class C amplifiers None of the mentione	are linear circuits, where the transistor is biase the input signal cycle. d	d to conduct	L1
23 Po a)	ower amplifiers in the Class A, B, C	increasing order of efficiency is:		L1

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24	 b) Class C, A, B c) Class B, A, C d) Efficiency of all the 3 If the output power of at 0.229 V given that the I a) 25% 	amplifiers is the same a amplifier is 10 V, and the input power supplied to the OC voltage used is 38.5 V, efficiency of the power amp	e amplif olifier is	ier is	
	 ⁴ b) 50% c) 75% d) 35% If a power amplifier has an output power of 10 W, and an amplifier gain of 16.4 dB, then the 				
25	input drive power is: a) 400 mW b) 225 mW c) 229 mW d) 240 mW				
26	Any device with negative a) Energy source b) Energy sink c) Oscillator d) None of the mentioned	e impedance as its characteristic property can be calle	d:	L2	
27	For achieving steady sta coefficients is: a) $_{in}= _L$ b) $_{in}=L$ c) $_{in}=1/_L$ d) None of the mentioned	te oscillation, the condition to be satisfied in terms of a	reflectio	50) et	
28	A one port oscillator use its desired frequency po a) -44+j123 b) 50+j100 c) -44+j145 d) None of the mentione	es a negative resistance diode naving _{in} =0.9575+j0.80 int. Then the input impedance of the diode is:		=50) at	
29	If the input impedance of impedance is to achieve a) 45-j23 b) -45+j23 c) 50 d) 23-j45	f a diode used in the microwave oscillator is 45-j23 stable oscillation is:	, then th	ne load	

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30	In a transistor amplifier, required to create enoug a) -84-j1.9 b) 28+j1.9 c) - (28+j1.9) d) None of the mentioned The phase variation for	if the input impedance is -84-j1.9 , then the the instability is:	terminating im	pedance L1
31	a) $f^*sin_m t/f_m$ b) f/f_m c) Sin_mt/f_m d) None of the mention	ed		L2
32	The expression for phase a) $_{rms}^{2}$ b) $_{rms}^{2}/2$ c) $_{rms}^{2}/2$ d) $_{rms}^{2}/3$	e noise in an oscillator is given by:		L4
33	A GSM cellular telepho signal levels of -23 dBm carrier, and -43 dBm at Determine the required a) -138 dBc/Hz b) -128 dBc/Hz c) -118 dBc/Hz d) None of the mentioned	ne standard requires a minimum of 9 dB reject a at 3 MHz from the carrier, -33 dBm at 1.6 MI 0.6 MHz from the carrier, for a carrier level of ocal oscillator phase noise at 3 MHz carrier fro mention Excellence for Empower d	ion of interferi Hz from the -99 dBm. equency offset	ng · L1
34	At higher frequencies of a) Thermal noise b) White noise c) Shot noise d) Flicker noise	operation of an oscillator, induced noise is mo		L2
35	 Phase noise at the output a) kBFGT₀ b) kT₀F/Pc c) kT₀F/Pc d) None of the mentioned 	t of an oscillator is given by: d		L3